SWIFT-UVOT-CALDB-##

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SWIFT UVOT CALDB RELEASE NOTE

SWIFT-UVOT-CALDB-##: Effective Area Curves

0. Summary:

This product provides the in-orbit effective area curves for the 7 filters of the UVOT.

1. Component Files:

| FILE NAME | VALID DATE | RELEASE DATE | VERSION |
|-----------|------------|--------------|---------|
| | | | |
| | | | |
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2. Scope of Document:

This document contains a description of the effective area curve calibration analysis performed to produce the effective area curve calibration products for the UVOT calibration database.

3. Changes:

This is the first release of the in-orbit effective area curves, replacing ground based calibration data.

4. Reason For Update:

An update was undertaken to improve the effective area curve calibration with in-orbit observations of known standard stars.

5. Expected Updates:

Further updates are expected following further analysis of PSF and coincidence loss correction.

6. Caveat Emptor:

The original ground-based effective area curves (SWIFT UVOTA calibration files: 20041116) were calculated incorrectly, therefore a comparison between these in-orbit curves and the ground-based curves in earlier versions of the CALDB is meaningless.

Due to the lack of faint spectroscopic standard stars, especially in the ultraviolet, the effective area curves have been calibrated with very few stars.

7. Data Used:

Observations of 4 white dwarfs and 2 Oke standard stars were taken in the UVOT filters. Where multiple observations were taken, images were spatially corrected and then co-added. Observation details, sorted by observation date, can be seen in Table 1.

| Object Name | Filter | Date | ID | Mode | Exposure |
|-------------|--------|------------|----------|------|------------|
| | | | | | Time (sec) |
| WD1657+343 | uvm2 | 25/02/2005 | 55900001 | Е | 707.01 |
| WD1657+344 | uvw1 | 25/02/2005 | 55900002 | Е | 572.35 |
| WD1657+343 | uvw2 | 25/02/2005 | 55900001 | Е | 740.79 |
| WD1657+343 | V | 25/02/2005 | 55900002 | Е | 605.79 |
| WD1121+145 | uvm2 | 04/03/2005 | 55250010 | Е | 671.82 |
| WD1121+145 | uvw1 | 04/03/2005 | 55250011 | Е | 139.61 |
| WD1121+145 | uvw2 | 04/03/2005 | 55250010 | Е | 715.78 |
| WD1121+145 | V | 04/03/2005 | 55250011 | Е | 412.77 |
| WD1121+145 | uvm2 | 05/03/2005 | 55250015 | Е | 753.42 |
| WD1121+145 | uvm2 | 05/03/2005 | 55250015 | I | 760.102 |

| WD1121+145 | uvw1 | 05/03/2005 | 55250017 | Е | 693.81 |
|--------------------------|--------------|------------|----------|---|---------|
| WD1121+145 | uvw1 uvw1 | 05/03/2005 | 55250017 | I | 699.719 |
| WD1121+145 | uvw2 | 05/03/2005 | 55250017 | E | 753.08 |
| WD1121+145 | uvw2 uvw2 | 05/03/2005 | 55250013 | I | 759.694 |
| WD1121+143 WD1657+343 | uvw2 uvm2 | 06/03/2005 | 55900018 | E | 693.04 |
| WD1657+343 | | 06/03/2005 | 55900018 | I | 698.704 |
| WD1657+343 WD1657+344 | uvm2 uvw1 | | 55900018 | E | 573.43 |
| | | 06/03/2005 | | | |
| WD1657+344 | uvw1 | 06/03/2005 | 55900020 | I | 580.012 |
| WD1657+343 | uvw2 | 06/03/2005 | 55900016 | E | 693.44 |
| WD1657+343 | uvw2 | 06/03/2005 | 55900016 | I | 700.201 |
| WD1121+145 | b | 05/04/2005 | 55250019 | I | 1045.97 |
| WD1657+343 | u | 12/04/2005 | 55900024 | I | 643.959 |
| WD1657+343 | V | 12/04/2005 | 55900025 | I | 640.45 |
| WD1121+145 | V | 13/04/2005 | 55250020 | I | 1577.75 |
| WD1121+145 | white | 10/05/2005 | 55250021 | I | 54.1386 |
| WD1657+343 | uvw2 | 19/06/2005 | 55900029 | I | 685.464 |
| WD1657+343 | b | 20/06/2005 | 55900030 | I | 951.898 |
| WD1121+145 | u | 20/06/2005 | 55250023 | I | 487.445 |
| WD1657+343 | white | 25/06/2005 | 55900032 | I | 157.362 |
| WD1026+453 | b | 07/07/2005 | 55761006 | I | 455.297 |
| sa95-42 | b | 07/07/2005 | 55763001 | I | 568.482 |
| sa95-42 | b | 07/07/2005 | 55763003 | I | 569.409 |
| WD0947+857 | b | 07/07/2005 | 55760005 | I | 395.554 |
| G24-9 | b | 07/07/2005 | 55762002 | I | 655.488 |
| WD1026+453 | u | 07/07/2005 | 55761005 | I | 290.699 |
| WD0947+857 | u | 07/07/2005 | 55760004 | I | 236.541 |
| WD1026+453 | uvm2 | 07/07/2005 | 55761004 | Е | 400.709 |
| WD0947+857 | uvm2 | 07/07/2005 | 55760002 | Е | 400.709 |
| WD0947+857 | uvw1 | 07/07/2005 | 55760003 | Е | 236.541 |
| sa95-42 | V | 07/07/2005 | 55763002 | I | 509.655 |
| sa95-42 | V | 07/07/2005 | 55763004 | I | 509.004 |
| G24-9 | V | 07/07/2005 | 55762001 | I | 1032.82 |

Table 1 – Table containing the observations used to calculate the in-orbit zero points. All of the sequence numbers in column 4 are missing their first three digits of 000. In column 5, I represents Image mode, and E represents Event mode

8. Description of Analysis:

The first step to calculating the in-orbit effective area curves was to correct the ground-based effective area curves. The in-orbit effective area curves were then calculated using in-orbit data analysis to update the new ground-based effective area curves.

8.1. Ground-Based Effective Area Curves

A smooth white filter effective area curve was created using a spline fit to the 6 ground-based filter points given in Table2. This smooth white filter curve is plotted in yellow in Figure 3.

| Filter | Wavelength (Å) | Effective Area (cm ²) |
|--------|----------------|-----------------------------------|
| UVW1 | 1930.0 | 86.26 |
| UVM2 | 2200.0 | 98.73 |
| UVW1 | 2600.0 | 106.73 |
| U | 3450.0 | 80.29 |
| В | 4370.0 | 47.17 |
| V | 5480.0 | 26.03 |

Table 2 - Ground-based calibration points.

The optical and UV filter ground-based effective area curves were calculated using the respective transmission filter curves seen in Figure 2. These transmission curves were then convolved with the white filter effective area curve (assuming that the white filter is transparent) to produce the ground-based effective area curves shown in Figure 3.

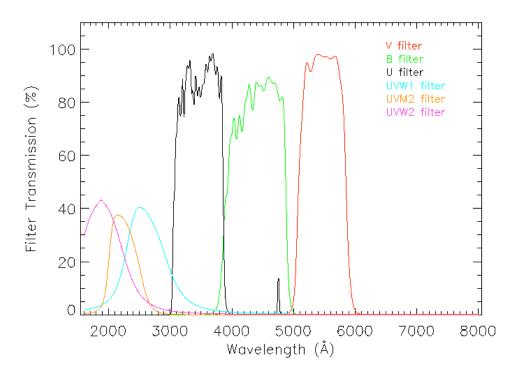


Figure 1 - Filter transmission curves.

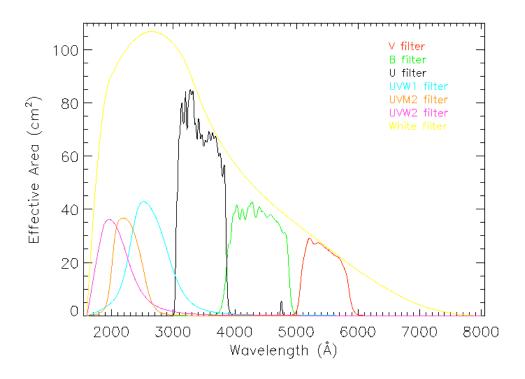


Figure 2 - Ground-based effective area curves.

Two methods were used to calculate the in-orbit effective area curves; one using count rate analysis, the other using zero point analysis. Due to the uncertainty of the ground based zero points, the in-orbit effective area curves were created using the count rate ratio method.

8.2. In-Orbit Effective Area curves

Observations of 4 white dwarfs and 2 Oke standard stars were taken in the UVOT filters (see Table 1 for details). Where multiple observations were taken, images were spatially corrected and then co-added. All observations were reprocessed using the latest CALDB teldef file (swugen20041120v102.teldef). The observed count rate was obtained using a 12 pixel (6 arcsec) aperture radius for optical filters and a 24 pixel (12 arcsec) radius for ultraviolet filters. All observed count rates were then corrected using the theoretical coincidence loss equation,

$$C_{theory} = \frac{-\ln(1 - C_{raw}ft)}{ft(1 - df)},$$

Where C_{theory} is the theoretically coincidence loss corrected count rate, C_{raw} is the raw observed count rate, ft is the frame time (0.011088s), and df is the deadtime fraction (0.0155844). This theoretical coincidence loss is then corrected by multiplying by the ground-based empirical formula,

$$f(x) = 1.0 + 0.2966x - 0.492x^2 - 0.4183x^3 + 0.2668x^4$$

Where $x = C_{raw} ft$.

The expected count rates of the 6 observed stars in each filter were obtained by convolving the known spectrum of each source with the new ground based effective area curves. The spectra of WD1657+343, WD0947+867 and WD1026+453 had to be extrapolated beyond 5700Å which will affect the V filter. The spectrum of WD1121+145 was complete across the wavelength range 1600-8000Å. The spectra of SA95-42 and G24-9 range from 3200-8000Å, which will affect all the UV filters and the U filter.

Tables 3 shows the results using these 6 observed stars, where C_{raw} is the raw observed count rate, T_{exp} is the total exposure time of the observation, C_{obs} is the coincidence loss corrected count rate, C_{exp} is the simulated count rate, and C_{ratio} is the ratio of observed to simulated count rates (C_{obs}/C_{exp}) .

| Source | Filter | T_{exp} | C_{raw} | C_{obs} | C_{exp} | C_{ratio} |
|------------|--------|-----------|----------------|---------------|-----------|-------------|
| | | (s) | (ph/s) | (ph/s) | (ph/s) | (ph/s) |
| WD1657+343 | V | 1246 | 3.56 ± 0.07 | 3.74 ± 0.07 | 4.88 | 0.77 |
| WD1657+343 | В | 952 | 13.11 ± 0.14 | 14.85±0.16 | 17.61 | 0.84 |
| WD1657+343 | U | 644 | 26.19±0.26 | 32.57±0.30 | 47.55 | 0.68 |
| WD1657+343 | UVW1 | 1726 | 30.37±0.14 | 38.80±0.21 | 60.87 | 0.64 |
| WD1657+343 | UVM2 | 2099 | 25.70±0.11 | 31.86±0.16 | 49.71 | 0.64 |
| WD1657+343 | UVW2 | 1426 | 44.30±0.18 | 61.47±0.36 | 71.07 | 0.86 |
| WD0947+867 | В | 396 | 24.51±0.32 | 27.55±0.37 | 33.88 | 0.81 |
| WD0947+867 | U | 237 | 49.24±0.50 | 58.93±0.65 | 89.71 | 0.66 |
| WD0947+867 | UVW1 | 237 | 57.61±0.51 | 70.34±0.71 | 109.81 | 0.66 |
| WD0947+867 | UVM2 | 401 | 48.05±0.35 | 57.34±0.46 | 88.45 | 0.65 |
| WD1026+453 | В | 455 | 17.46±0.25 | 19.26±0.29 | 24.79 | 0.78 |
| WD1026+453 | U | 291 | 34.05±0.37 | 39.23±0.45 | 62.45 | 0.63 |
| WD1026+453 | UVM2 | 401 | 47.84±0.35 | 57.07±0.46 | 58.32 | 0.98 |
| WD1121+145 | V | 2678 | 2.87±0.05 | 2.99±0.05 | 3.36 | 0.89 |

| WD1121+145 | В | 1046 | 11.13±0.13 | 12.41±0.15 | 12.08 | 1.03 |
|------------|------|------|------------|------------|-------|------|
| WD1121+145 | U | 487 | 21.07±0.23 | 25.30±0.31 | 36.81 | 0.68 |
| WD1121+145 | UVW1 | 1533 | 25.88±0.14 | 32.12±0.19 | 49.06 | 0.65 |
| WD1121+145 | UVM2 | 2185 | 21.50±0.10 | 25.89±0.13 | 40.77 | 0.88 |
| WD1121+145 | UVW2 | 2229 | 36.04±0.13 | 47.68±0.22 | 56.22 | 0.85 |
| SA95-42 | V | 1019 | 7.54±0.13 | 8.16±0.14 | 11.16 | 0.73 |
| SA95-42 | В | 1138 | 24.05±0.18 | 29.48±0.26 | 36.24 | 0.81 |
| G24-9 | V | 1033 | 6.95±0.10 | 7.49±0.16 | 9.30 | 0.80 |
| G24-9 | В | 655 | 13.85±0.17 | 15.77±0.22 | 17.90 | 0.88 |

Table 3 - Count Rate results for WD1657+343, WD0947+867, WD1026+453, WD1121+145, SA95-42 and G24-9.

8.3. Comparing the Ratio Results

The average ratios can be seen in Table 4, along with the ratio results for WD1657+343, WD0947+867, WD1026+453, WD1121+145, SA95-42 and G24-9.

| Filter | Count | Count | Count | Count | Count | Count | Aver. |
|--------|--------|--------|--------|--------|---------|-------|---------------|
| | Rate | Rate | Rate | Rate | Rate | Rate | Ratio |
| | Ratio | Ratio | Ratio | Ratio | Ratio | Ratio | |
| | WD1657 | WD0947 | WD1026 | WD1121 | Sa95-42 | G24-9 | |
| | +343 | +867 | +453 | +145 | | | |
| V | 0.77 | - | - | 0.89 | 0.73 | 0.80 | 0.80 ± 0.07 |
| В | 0.84 | 0.81 | 0.78 | 1.03 | 0.81 | 0.88 | 0.86 ± 0.09 |
| U | 0.68 | 0.66 | 0.63 | 0.68 | - | 1 | 0.66 ± 0.02 |
| UVW1 | 0.64 | 0.64 | - | 0.65 | - | 1 | 0.64 ± 0.01 |
| UVM2 | 0.64 | 0.65 | 0.98 | 0.88 | - | - | 0.77±0.17 |
| UVW2 | 0.86 | - | - | 0.85 | - | - | 0.86 ± 0.01 |

Table 4 - Ratio results used to produce the in-orbit effective are curves.

Figure 4 shows the comparison between the in-orbit effective area curves using the average count rate ratios (solid lines), and the ground based effective area curves (dashed lines).

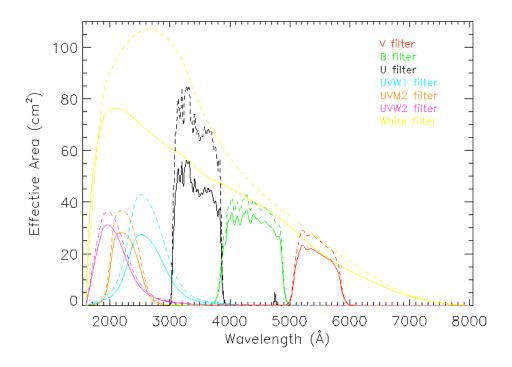


Figure 3 - Effective area curves using the average count rate ratio. Solid lines are in-orbit curves, dashed lines are ground-based curves.

8.4. Predicted Effective Area Curves

Predicted effective area curves were created by considering the known responses of the UVOT detector and filters in the wavelength region 1600Å to 8000Å. The following were considered when calculating the predicted effective area curves:-

- 1. Transmission curves for each filter
- 2. Quantum efficiency of the photon counting system (D.Q.E)
- 3. Mirror reflectivity
- 4. Telescope area (596cm²)

Figure 6 shows the predicted effective area curves produced by convolving these sub-component measurements using,

EffectiveAreaCurve = $Transmission \times DQE \times MirrorReflectivity^3 \times 596$,

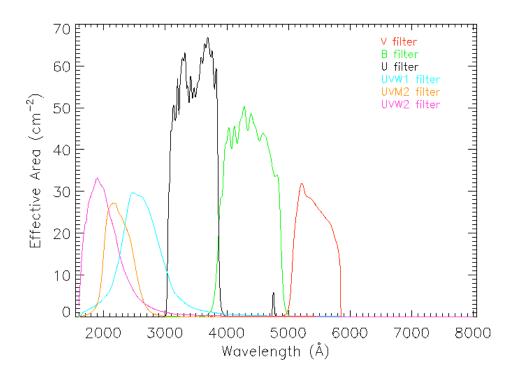


Figure 4 - Predicted effective area curve for UVOT.

8.5. Comparing the different Effective Area Curves

Table 5 shows the ratios of in-orbit to ground (Column 2), ground to predicted (Column 3), and in-orbit to predicted (Column 4) ratios. Errors in the ground-based measurements and instrument responses are not taken into account here, but will add uncertainty to these results (the error in the D.Q.E. measurement is up to 10%). The plots of these comparisons can be seen in Figures 3, 5 and 6 respectively.

| Filter | In-Orbit/Ground | Ground/Predicted | In-Orbit/Predicted |
|--------|-----------------|------------------|--------------------|
| V | 0.80±0.07 | 0.99 | 0.79 |
| В | 0.86±0.09 | 0.88 | 0.76 |
| U | 0.66±0.02 | 1.22 | 0.80 |
| UVW1 | 0.64±0.01 | 1.34 | 0.89 |
| UVM2 | 0.77±0.17 | 1.37 | 1.05 |
| UVW2 | 0.86±0.01 | 1.14 | 0.97 |

Table 5 - Ratio results when comparing predicted, in-orbit and ground-based effective area curves.

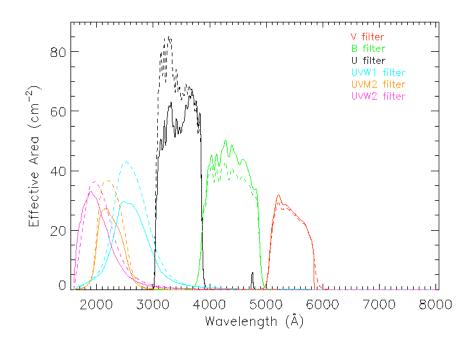


Figure 5 - Comparison of predicted effective area curves (solid lines) to ground-based effective area curves (dashed lines).

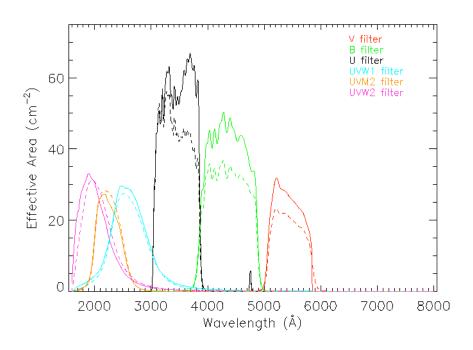


Figure 6 - Comparison of predicted effective area curves (solid lines) to in-orbit effective area curves (dashed lines).

Figure 5 and Table 5 show that in the case of the ultraviolet and the U filters, the ground-based effective area curves are higher than expected from the predicted data. This suggests there may either be a problem with the ground-based calibration, or there is something missing in the predicted data. Figure 5 also shows that the V filter ground-based calibration agrees with the predicted, but there is a decrease in the B filter ground-based calibration compared to the predicted results.

Figure 6 and Table 5 show that in general, the in-orbit effective area curves have decreased when comparing to the predicted curves. The optical filters show a greater decrease than the UV filters. We also see this larger decrease in the optical when comparing the ground-based and in-orbit zero points.